

Enhancing Heat Transfer Rate by Optimization of Commercial Refrigeration Condenser and its Design Metrics

N. Venkateswara Rao

*Department of Mechanical Engineering
Chaitanya Bharathi Institute of Technology, Gandipet, Hyderabad-75, India*

Narasimha Kulkarni

*Department of Mechanical Engineering
Chaitanya Bharathi Institute of Technology, Gandipet, Hyderabad-75, India*

K. Y. Sreeram

*Department of Mechanical Engineering
Chaitanya Bharathi Institute of Technology,
Gandipet, Hyderabad-75, India
Corresponding Author

Abstract

Optimization of Heat transfer rate & size of Heat money changer (condenser) by 2 significant tests met by Refrigeration structure proposals. The Heat transfer rate problem is concerned with the determination total heat transfer rate, and the sizing issues worried for those determination of the aggregate high temperature exchange surface range. The key element helping for higher heat exchange rate & base high temperature exchange zone may be those refrigerant streams out in the condenser coil, likewise those framework lies over indoor of a bureau. The objective of the available task is will streamline those outlined of a commercial refrigeration condenser to enhancement the heat transfer rate. CFD (Computational Fluid Dynamics) and Condenser software will be used to optimize the design of the components. Structural dissection about parts will be also will be performed with dissect the deformations & anxieties happening because of weights & temperatures of the stream. The necessary modifications are made to improve the heat transfer rate & reduce size of condenser that enhances the overall heat transfer rate.

Keywords: Condenser design, Refrigeration, condenser circuit, CAD & Analysis.

1. Introduction

The main objective of this Project is to reduce size of the condenser and enhance the heat transfer rate. The Condenser is a device which used to exchange the heat absorbed to ambient. It rejects heat to external cooling medium (air or water). May be those procedure of evacuating high temperature from an encased space, or from An substance, Furthermore moving it will a spot the place it camwood a chance to be excluded in high face area, low FPI & optimum refrigerant flow through condenser coil and air flow over the condenser coil are the key for effective condenser performance.

In the present study, the condenser coil circuit is optimized so that the refrigerant flow through the condenser flows via two tubes parallels and the heat exchange between the refrigerant and the external surface occurs very quickly.

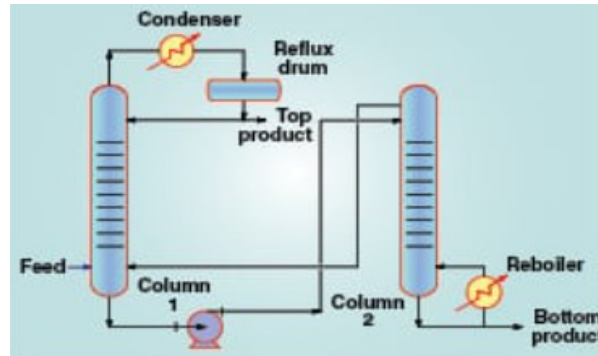


Fig.1 Detail explanation of Condenser with phase change.

2. Experimental Setup of Condenser Optimization

The issues that mainly effect the heat transfer rate in a required convection type condenser

2.1 Air Cooled Condenser Selection

Air cooled condenser might be common convection sort alternately constrained convection sort. In practically as a relatable point we utilize air cooled condenser. In front of measuring a condenser, cautious assessment of the necessities for a particular establishment will be fundamental. The assessment ought to include, attention from claiming starting cost, operating cost, administration an aggregation Furthermore kind about load. A condenser that is excessively little camwood make unreasonable What's more make operating issues in easier encompassing states a under-size condenser camwood make working issues in higher encompassing states. It is, therefore, paramount with think about those taking after factors in front of measuring a condenser:

1. Terrible heat dismissal.
2. Encompassing temperature.
3. Consolidating temperature.
4. Temperature distinction (TD).
5. Wind stream.

Condenser ability is a capacity of the essential high temperature exchange equation.

$$Q_c = U \times A \times LMTD$$

here

$$Q_c = \text{Condenser capacity in Cal/hr (Ref. effect + Heat of Comp + Motor winding heat)}$$

$$U = \text{Overall heat transfer coefficient K.Cal/m}^2\text{Hr.}^\circ\text{C A}$$

$$= \text{Effective surface area in m}^2$$

$$LMTD = \text{Log mean temperature difference between the condensing refrigerant and the condensing medium in }^\circ\text{C}$$

$$\text{Face area} = \text{Air quantity} / \text{Air velocity}$$

The greatest speed happens between those tubes since the tubes blockan and only those streams acceptably. If B is those dividing among tubes in the face and c may be the tube dividing among rows, also d may be those tube breadths. The Reynolds and Nusselt number are defined as follows for this case:

$$Re = (\rho \times d_o \times U_\infty) / \mu$$

The Grimson's correlation is as follows

Where the constants C and n are dependent upon Reynolds number.

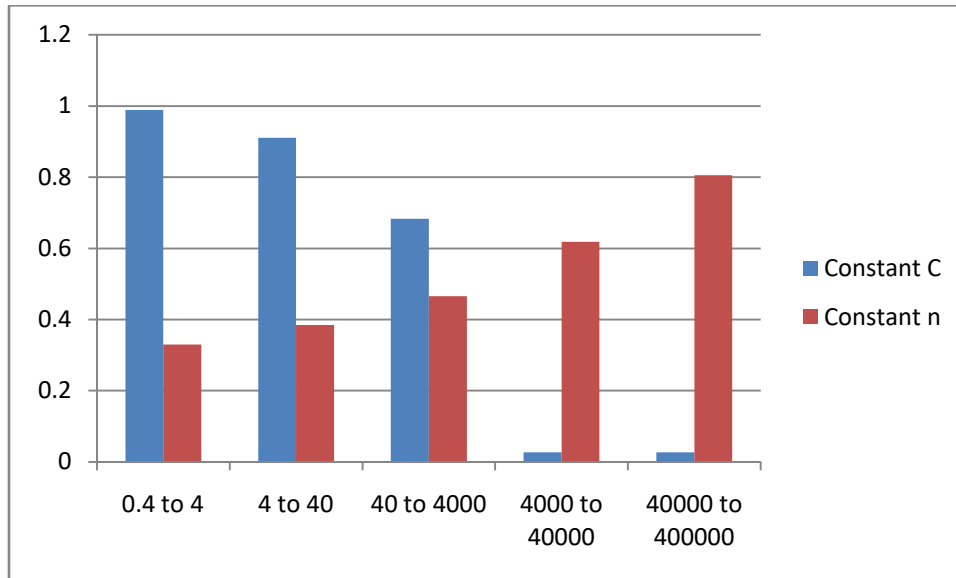


Figure.2. Constant for Grimson's Equation

Design of Condenser

Design Considerations

- Tube Size : 3/8th
- Outside diameter of the condenser tube : 0.0079
- Inside diameter of the condenser tube : 0.0068
- Refrigerant used : R404A
- Evaporator Temperature(°C) : 7.2
- Condenser Temperature(°C) : 54
- Sub cooling Temperature(°C) : 10
- Super heating Temperature(°C) : 10.8
- Compressor Power(W) : 678
- Cooling Capacity(Btu/hr) : 5460
- Ambient Temperature(°C) : 43

Enthalpy values taken from P-h chart

$$H_1=400\text{KJ / Kg } H_4=270\text{KJ / Kg } H_2 =430 \text{ KJ / Kg } H_5=245 \text{ KJ / Kg } H_3 =420 \text{ KJ / Kg } H_6=245 \text{ KJ / Kg}$$

$$\text{Refrigerant Effect} = H_1 - H_6$$

$$= 155 \text{ KJ / Kg}$$

$$\text{HeatRejectionCapacity (HRC)} = (\text{Refrigeration capacity} * \text{power of compressor}) * \text{FOS}$$

$$= ((1.6) + (678/1000)) * 1.05 = 2.392 \text{ KW}$$

Overall heat transfer coefficient

$$1/U_o = (A_t/A_j) * (1/h_i \text{ condensation}) + 1/h_o \quad U_o = 47.46 \text{ W/m}^2 \text{ K}$$

$$\text{LMTD condensation} = 7.61 \text{ }^\circ\text{C}$$

2.2 CAD Modeling

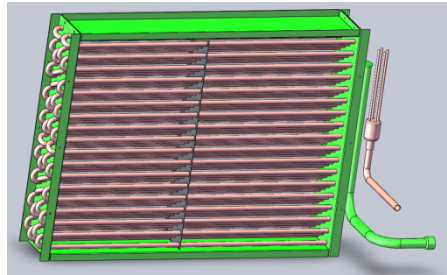


Figure.3. Existing design with 12 tube single circuit

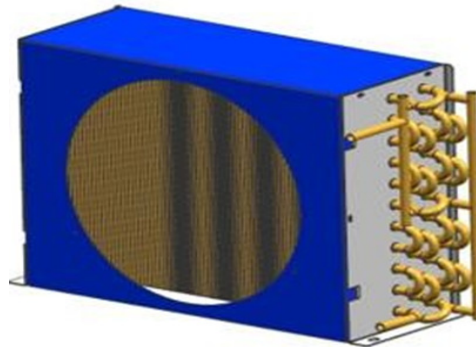


Figure.4. New design with 11 tube

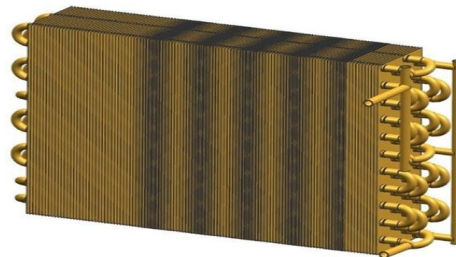


Fig. 5, Condenser coil with fins

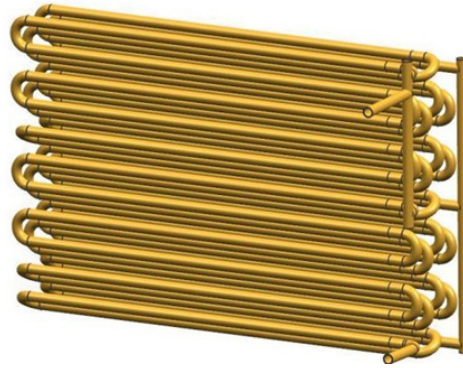


Fig. 6. Condenser coil without fins



Figure.7. Physical model of the design

2.3 ANALYSIS Structuralanalysis

Boundary Conditions:

Inlet: Temperature: 85 [C°]

Outlet: Mass flow rate = 0.0137(kg/s) Ref. Pressure: 14.7[PSI] Assumptions: Steady state single phaseanalysis.

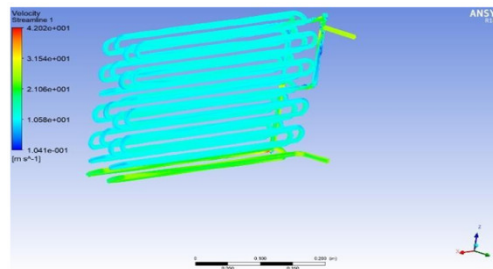


Fig. 8. 11*4 Row Condenser VelocityStreamlines

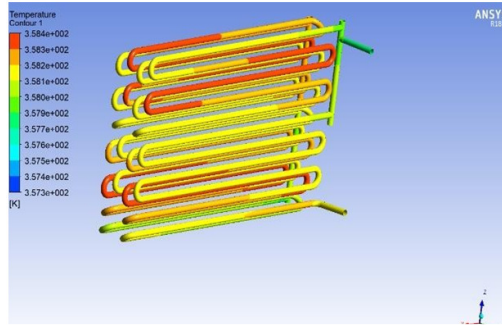


Fig.9. Temperature contour

	inlet	outlet
MFR	1.370e-02 [kg s ⁻¹]	-1.370e-02 [kg s ⁻¹]
Velocity	2.751e+01 [m s ⁻¹]	2.327e+01 [m s ⁻¹]
Temp	3.581e+02 [k] (84.95 Deg.c)	3.177e+02 (44.55 Deg.c)

Table.2. Velocity and Temperature

Results and Discussion

By comparing the two models the outlet temperature of the new design is better. By optimizing the circuit design from one circuit to two circuit the Heat transfer rate of the condenser is improved by 6% though the height of the condenser is decreased by 9 % by reducing one row of tube. The Capacity increased from 3.17 KW to 3.37 KW. With this achievement the higher capacity of compressor can be used for the same refrigeration system and can be used in the very compact sized refrigeration units. The above data is calculated from the LUVATA Thest Condenser design Software and the images of the same are shown below

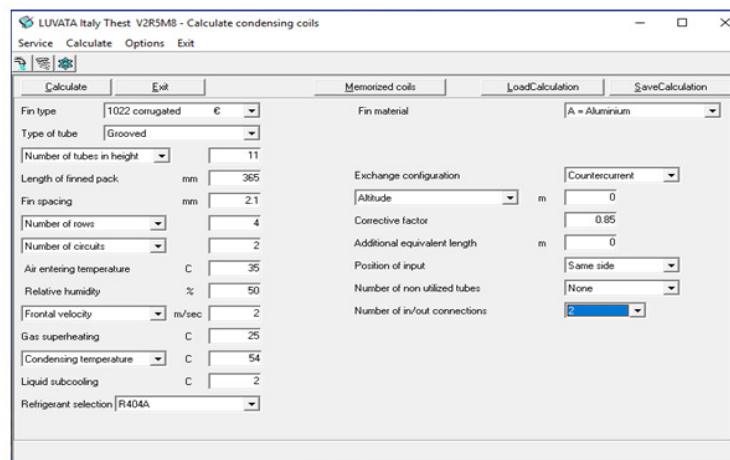


Fig.10. Input for 11 Tubes Condenser

Output Video			
ECC code 1022A1104036521C00(1+1)			
Fin type	25 X 21.65 Staggered	1022 corrugated	1022c (STD)
Type of tube	9.21 Grooved C		
Fluid	R404A		
Utilized tubes	44	HxLxP [mm]	275 x 365 x 87
Non utilized tubes	0	Outer area [m ²]	7.53
Inner volume [l]	1.18	Frontal area [m ²]	0.1
Headers		Inner area [m ²]	0.465
Tubes per circuit	22		
AIR SIDE		SIDE -R404A	
Entering temp. [°C]	35	Delta superheating [°C]	25
U.R. entering [%]	50	T. condensing gas [°C]	54
Outlet temp. [°C]	49.5	T. condensing liq. [°C]	53.9
U.R. outlet [%]	23.4	Delta subcooling [°C]	2
Flow [m ³ /h]	722.7		
Flow [kg/s]	0.224		
Frontal velocity [m/s]	2	Total flow [kg/h]	81.8
Pressure drop [Pa]	38.1		
Barometric pres. [kPa]	101.325	Coil pressure drop [kPa]	6.53
Altitude [m]	0	Pressure sat [bar]	24.9
Type of calculation	Countercurrent	Total capacity [kW]	3.37
Corrective factor	0.85		
Additional equivalent length	0		

Fig.11. Output for 11 Tubes Condenser

Conclusion

By optimizing the circuit designs from one circuit to two circuits the Heat transfer rate of the condenser is improved by 6% though the size of the condenser is decreased by 9 % by reducing one row of tube. The Capacity increased from 3.17 KW to 3.37 KW. With this achievement the higher capacity of compressor can be used for the same refrigeration system and can be used in the very compact sized refrigeration units. With this new design the cost of the unit can be reduced by about 5 to 6%. In conclusion, by optimizing the circuit design the performance of the condenser can be improved

References

1. Y Peng¹, S J Zhang^{1,3}, F Shen¹, X B Wang², X R Yang² and L J Yang². IOP Conf. Series: Earth and Environmental Science 93 (2017)012067.
2. Mallikarjun¹, Anandkumar S Malipatil ² Volume 2 Issue X, October 2014 ISSN: 2321-9653 International Journal for Research in Applied Science & Engineering Technology(IJRASET)
3. A. Kalendar, T. Galal*, A. Al-Saftawi, M.Zedan S. S. Karar and R. El-shiaty Department of Mechanical & Refrigeration Engineering, College of Technological Studies, PAAET, Kuwait
4. Firoz Rangrez¹, Prof. S.H.Kulkarni² Department of Mechanical Engineering, Mumbai University VeermataJijabai Technological Institute, Mumbai, Maharashtra, India International Journal of Emerging Technologies in Computational and Applied Sciences (IJETCAS) 14-450; © 2014, IJETCAS
5. Webb R L (1994) Principles of Enhanced Heat Transfer, John Wiley & Sons Inc, New York.
6. Han JC, Glicksman LR, Rohsenow WM (1978) An Investigation of Heat Transfer and Friction for Rib-Roughened Surfaces, Int J Heat Mass Transf 21:143-1156.
7. Webb RL (1979) Toward a Common Understanding of the Performance and Selection of Roughness for Forced Convection. Studies in Heat Transfer: A Festschrift for E.R.G. Eckert, J.P. Hartnett et al., Edn,

Hemisphere Publishing Corp, Washington:257-272.

8. Fenner GW, Ragi EG (1979) Enhanced Tube Inner Surface Heat Transfer Device and Method,USA.
9. 5. Gee DL, Webb RL (1980) Forced Convection Heat Transfer in Helically Rib Roughened Tubes. Int J Heat Mass Transf 23:1127-1136.
10. Yerrennagoudaru, H, & KB, K. S., Effect of Nozzle Holes and Turbulent Injection on